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REPORT NO. STI TR 10255 VOL I

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# NAVSTAR GLOBAL POSITIONING SYSTEMS SPECIAL STUDIES AND ENGINEERING PROGRAM

VOLUME I

**FINAL REPORT** 

Prepared by:

James J. Spilker, Jr.
Lloyd Engelbrecht
Jackson T. Witherspoon

October 25, 1975



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SPACE AND MISSILE SYSTEMS ORGANIZATION (AFSC)
LOS ANGELES AIR FORCE STATION
LOS ANGELES, CALIFORNIA

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# NAVSTAR GLOBAL POSITIONING SYSTEMS SPECIAL STUDIES AND ENGINEERING PROGRAM

VOLUME I FINAL REPORT

#### GPS/SAC BOMB SCORING SYSTEM EVALUATION

Prepared by:

James J. Spilker, Jr.
Lloyd Engelbrecht
Jackson T. Witherspoon

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#### **FOREWORD**

This document is Volume I of a four volume report. The four volume report is titled, "NAVSTAR Global Positioning Systems Special Studies and Engineering Program". Volume I summarizes the work performed for the Air Force and specifically addresses the GPS/SAC Bomb Scoring System Evaluation. It was previously submitted in draft form on October 15, 1975, under report number STI/GPS-052.

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#### SECTION 1

#### BOMB SCORING SYSTEM EVALUATION

#### 1.0 INTRODUCTION

### 1.1 General

This report describes the evaluation and comparison of three Bomb Scoring System (BSS) techniques which use the GPS satellites to assist in the accuracy assessment. The objective of each system is to provide an independent evaluation of the aircraft's navigation/bombing accuracy and is therefore supplemental to the aircraft's navigation system.

Alternate A considers the use of on-board GPS and other aircraft instrumentation to derive the evaluation. Since it uses on-board equipment, alternate A has the least impact on the aircraft's performance. It is of course limited in its application to GPS-equipped aircraft.

Alternate B considers the use of totally redundant equipment, carried in a separate BSS pod to derive the independent assessment, and is similar in nature to the GPSTP.

Alternate C considers the use of transponded data to a ground station in order to minimize the aircraft-carried equipment therefore minimizing the impact to the aircraft's performance. Prior investigation has shown that the accuracy requirements can be achieved using this concept.

<sup>\*</sup>STI report "GPS/SAC System Concept" dated April 8, 1975.

Sections 2, 3, and 4 describe the alternates A, B, and C respectively and define the impact of each approach on the aircraft and also provide ROM cost estimates for each approach. Section 5 compares the techniques and delineates the recommendations.

## 1.2 Summary Conclusions

#### 1.2.1 Alternate A

Alternate A, while being the least costly and also minimizing the impact on the aircraft, is least flexible and does not satisfy the BSS assessment capability for non-GPS equipped aircraft. It is therefore not a stand-alone solution and is not recommended.

#### 1.2.2 Alternates B, C

Alternate C is approximately equivalent to Alternate A in its minimal impact on the aircraft, but provides for significantly improved flexibility in utilization over Alternate A. Additionally, Alternate C provides the excellent opportunity for real-time assessment, a capability not easily achieved with alternates A or B. Alternate C costs are approximately equal to Alternate B if two pods are implemented, and becomes more economical than B if more than two pods are implemented. Alternate C is the recommended approach.

Cha	Characteristics	Alternate A (X-Set Equipped A/C)	Alternate B (X-Set in BSS Pod)	Alternate C (Transponded Signals
<b>bhk</b> eic <b>y</b> e	Aircraft weight power size	430 lbs. 485 watts small pod	1135 lbs. 1515 watts large pod (600 gal)	536 lbs. 480 watts small pod
	Capable of Real Time Assessment	ou	ou	yes(added processor required)
TVNC	Adaptable to wide variety of aircraft	no (mư. j have X-set)	yes (must have capa- bility of carrying pod)	yes
OPERATIO	Independent of Target Location	yes	yes	no (Aircraft must be in range of ground terminal: 80 nmi at 5000 ft. altitude)
	Independent Assessment	no (uses same navigation data as aircraft)	yes	yes
<b>PERFORMANCE</b>	Ability to Resolve Ionos- pheric Propagation Errors	excellent	excellent	<pre>good (requires inter-    polation from    ground terminal/    satellite    geometry to    aircraft/satellite    geometry)</pre>
J	1 Pod	\$550 K	\$1,190 K	\$1,430 K
LSO	2 Pods	\$715 K	\$1,735 K	\$1,665 K
0	3 Pods	\$880 K	\$2,280 K	\$1,900 K

#### SECTION 2

#### 2.0 ALTERNATE A - USE OF ON-BOARD X-SET DATA

### 2.1 System Description

Alternate A has been considered for the Bomb Scoring System (BSS) because it requires the minimum additional hardware and aircraft modification for those aircraft already equipped with the X-set user equipment. Figure 2-1 shows the system equipment configuration.

In normal operation, the aircraft receives the L1 and L2 signals from multiple satellites to determine its position. Both L1 and L2 are received to resolve the i nospheric propagation error. Figure 2-2 shows the signal spectra. The signals are acquired by the X-set receiver, and the data and timing signals are fed to the X-set data processor. Figure 2-3 is a block diagram of the user X-set, and Figure 2-4 shows the interface of the instrumentation processor with the X-set.

The X-set processor data, the bombing mission events, and IRIG time are also fed to the instrumentation processor for formatting and then fed to the digital tape recorder.

## 2.2 System Characteristics

while Alternate A applications are limited to only those aircraft already equipped with the GPS/X-set equipment, the system does provide a low cost assessment capability. The system can be utilized on any selected range (i.e. the system is not "tied" to the ground station). Aircraft frame modifications are minimal in that only the interface cabling must be added.

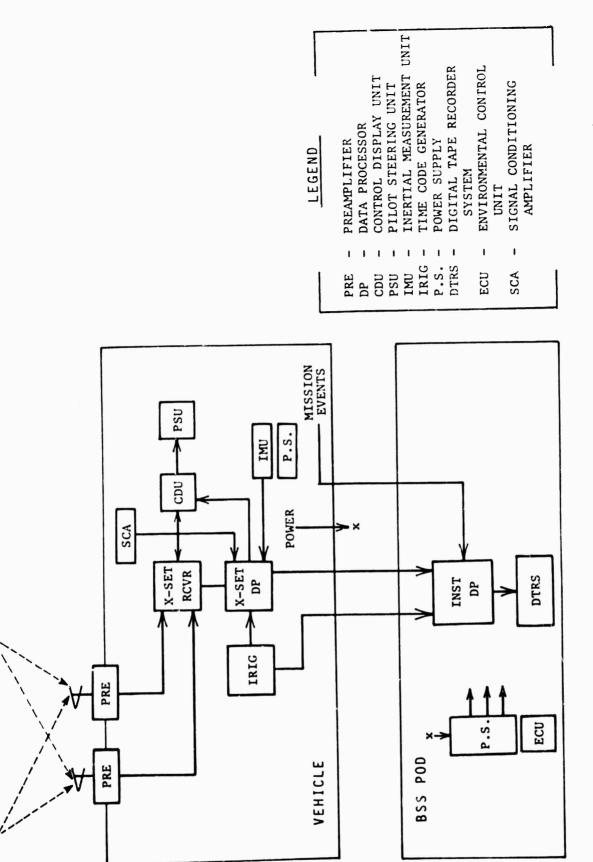


FIGURE 2-1 ALTERNATE A CONFIGURATION (Use of Vehicle X-Set)

Figure 2-2 Navigation Signals

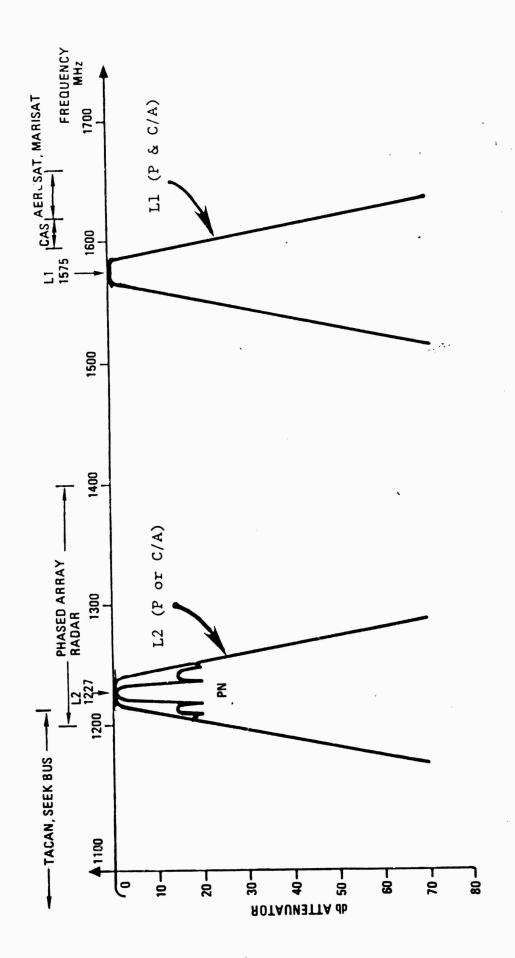
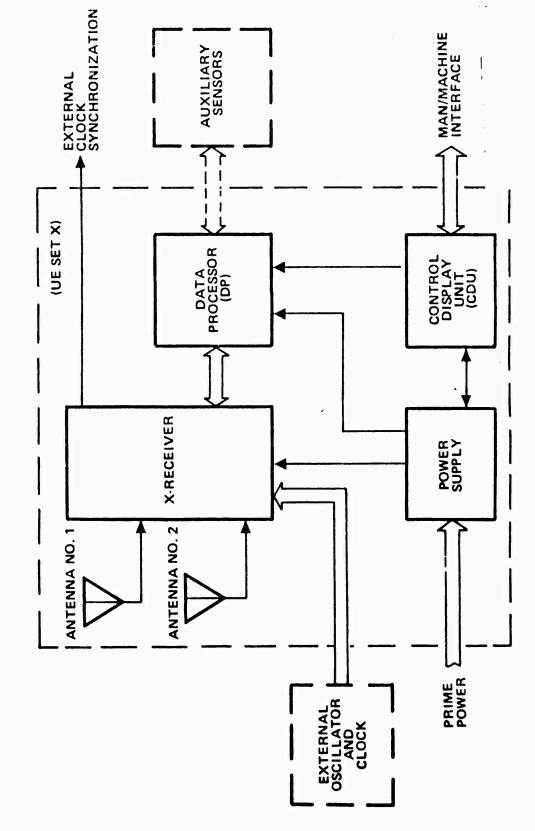
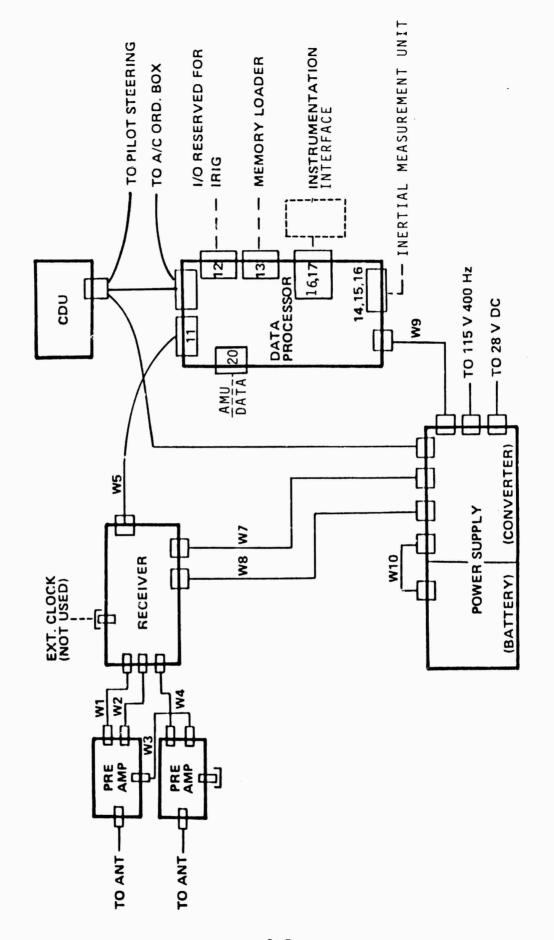


Figure 2-3

UE SET X PRIME ITEM FUNCTIONAL BLOCK DIAGRAM



X SET (UNAIDED) USER EQUIPMENT



=

Table 2-5 summarizes the estimated weight, volume and power requirements for alternate A. Table 2-6 is a ROM cost tabulation for the implementation.

TABLE 2-5

## ALTERNATE A

# EFFECT ON AIRCRAFT

AIRCRAFT	WEIGHT	VOLUME	POWER
Cabling	10 lbs	300 in <sup>3</sup>	-
BSS POD			
Instrumentation D.P Recorder P.S. E.C.U. Subtotals Pod Hardware Subtotals Pod and Pod Adapter Cables BSS TOTAL	44.9 lbs 40.1 lbs 40 lbs 40 lbs 165.0 lbs 25.0 lbs 190.6 lbs 200 lbs 30 lbs 420 lbs	3253 in <sup>3</sup> 1407 in <sup>3</sup> 2000 in <sup>3</sup> 3000 in <sup>3</sup> 9660 in <sup>3</sup>	175 watts 100 watts 200 watts 10 watts 485 watts
TOTAL IMPACT	430 lbs		485 watts

TABLE 2-6

# ALTERNATE A

# ROM COST IMPACT

AIRCRAFT MODIFICATIONS	NON-RECURRING	RECURRING
Cabling/Install/Doc/Test	\$ 10,000	\$ 10,000
BSS POD		
Instrumentation D.P/Software	\$100,000	\$ 35,000
Recorder	10,000	25,000
E.C.U.	50,000	20,000
P.S. System/Panel	25,000	20,000
Pod Modifications/Doc.	50,000	20,000
Integrate/Install/Test	15,000	25,000
SYSTEM		
Test	\$ 25,000	\$ 10,000
AGE	100,000	-
TOTALS	\$385,000	\$165,000

#### SECTION 3

#### 3.0 ALTERNATE B - X-SET IMLPLEMENTATION IN GPSTP

### 3.1 System Description

Alternate B consists of a BSS pod utilizing an X-set for independent position assessment. This alternative requires only that antennas and preamps be installed on the host aircraft for the reception of NAVSTAR Ll and L2 signals. Figure 3-1 shows the Alternate B configuration which is essentially the same configuration as the GPSTP configuration.

The L1 and L2 signals are received via antennas and preamplifiers installed on the host vehicle. These signals, plus power, and bomb release data are fed to the BSS pod. The BSS pod contains the user X-set equipment, the inertial measurement unit, air temperature sensor for the air mass measurement, IRIG time, the instrumentation processor, and digital tape recorder. Additionally, a power supply subsystem and environmental control unit are required.

# 3.2 System Characteristics

Alternate B is applicable to a wide variety of aircraft whether equipped with GPS navigation equipment or not, and additionally, this alternative is not constrained to a range limitation (i.e. system is not "tied" to a ground station). Table 3-2 is a summary of the weight, volume, and power impact and Table 3-3 is a ROM estimate of the System's implementation.

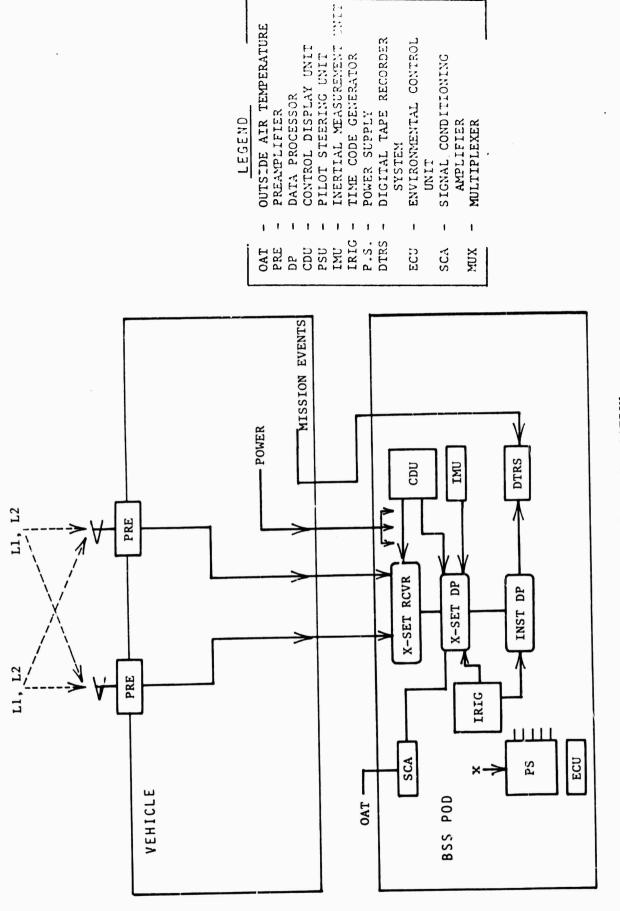


FIGURE 3-1 ALTERNATE B CONFIGURATION (X-Set Supplied in BSS POD)

-2

# TABLE 3-2

## ALTERNATE B

# CHARACTERISTICS

AIRCRAFT	WEIGHT	VOLUME	POWER
Antenna/Preamp	30 lbs	700 in <sup>3</sup>	3 watts
BSS POD			
X-Set (Total) Instrumentation D.P. IRIG TEG I.M.U. DTRS DAT/SCU Subtotal P.S.S E.C.U. Pod Hardware Subtotal Pod/Pod Adapter Cables POD TOTAL	226 lbs 45 lbs 15 lbs 34 lbs 41 lbs 2 lbs 363 lbs 90 lbs 120 lbs 85 lbs 658 lbs 385 lbs 60 lbs 1103 lbs	9,338 in <sup>3</sup> 3,253 in <sup>3</sup> 973 in <sup>3</sup> 1,496 in <sup>3</sup> 1,407 in <sup>3</sup> 12 in <sup>3</sup> 16,479 in <sup>3</sup> 4,400 in <sup>3</sup> 8,000 in <sup>3</sup>	775 watts 175 watts(est) 40 watts 100 watts(est) 100 watts 1 watt 1190 watts 300 watts 20 watts
AIRCRAFT TOTAL	1133 lbs		1513 watts

TABLE 3-3
ALTERNATE B
ROM COST IMPACT

Aircraft Frame	Non-Recurring	Recurring
Ant/Install	\$ 50,000	\$ 10,000
Reamp/Install	-	30,000
Intg/DOC	20,000	-
Test	10,000	5,000
BSS POD		
X-Set	-	150,000
Inst. D.P. (Soft)	100,000	35,000
IMU	-	100,000
DTRS	10,000	25,000
IRIG TCG	-	20,000
OAT/SCA	-	10,000
ECU	50,000	30,000
P.S. SYSTEM/PANEL	30,000	25,000
POD MODIF/DOC	150,000	40,000
INTEG/INSTALL/TEST	35,000	40,000
SYSTEM		
TEST	40,000	25,000
AGE	150,000	-
TOTAL	\$645,000	\$545,000

#### SECTION 4

- 4.0 ALTERNATE C TRANSPONDED SIGNALS
- 4.1 System Description

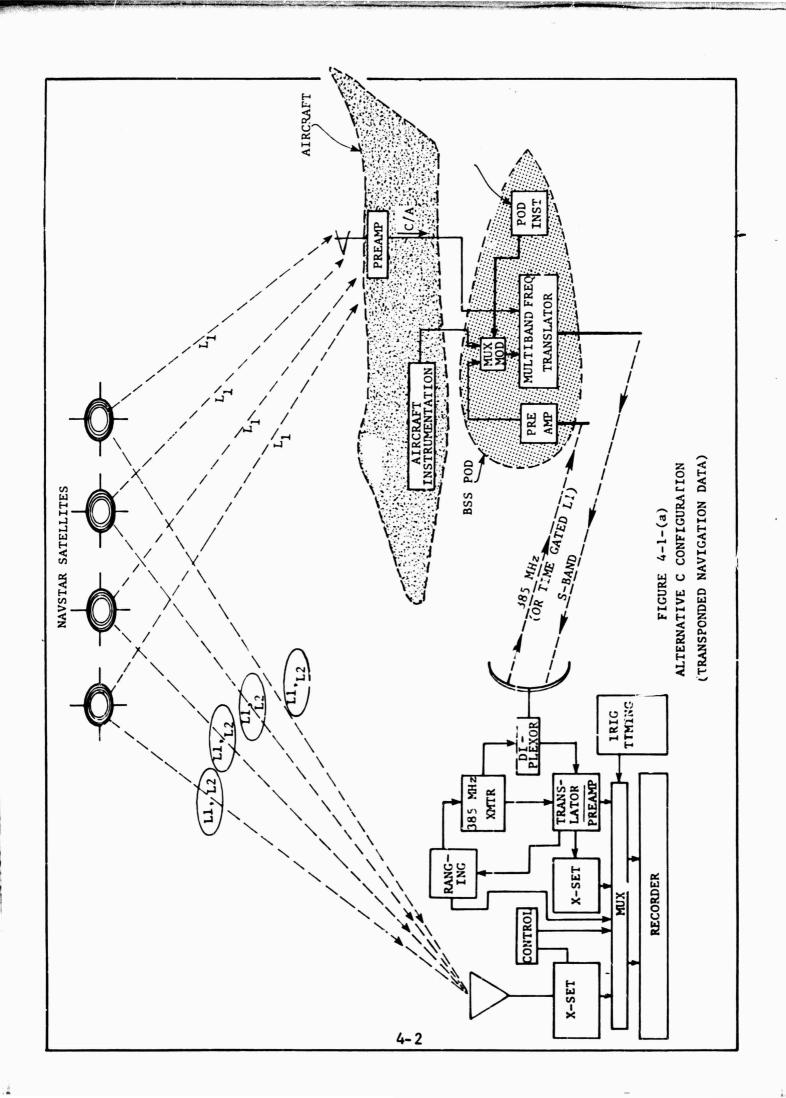
Figures 4-1 (a) and (b) are block diagrams of a Bomb Scoring System utilizing aircraft and navigation data transponded to a ground station. The satellite L1 and L2 signals are received by the ground stations to precisely determine its position, and the signals are also used as reference signals for the aircraft relayed navigation signals.

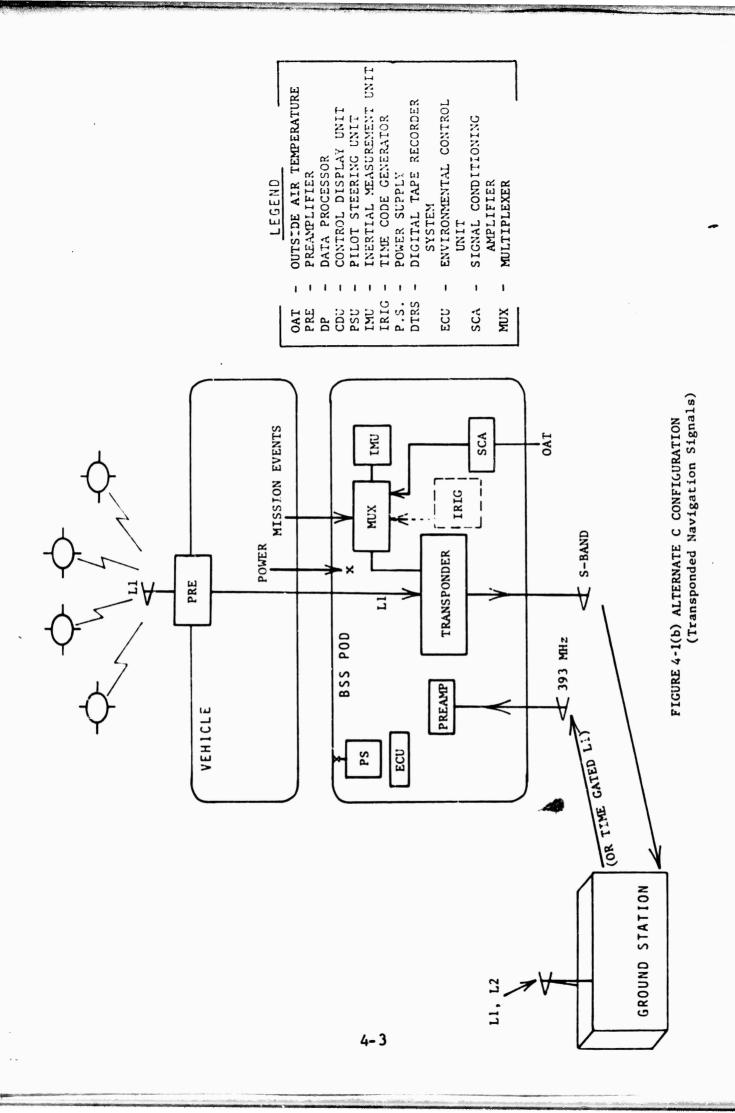
The aircraft receives the Ll signals, amplifies and frequency translates them, and transmits the signals to the ground station. The differential delay of each signal relative to the direct signal permits the ground station to compute the aircraft's position.

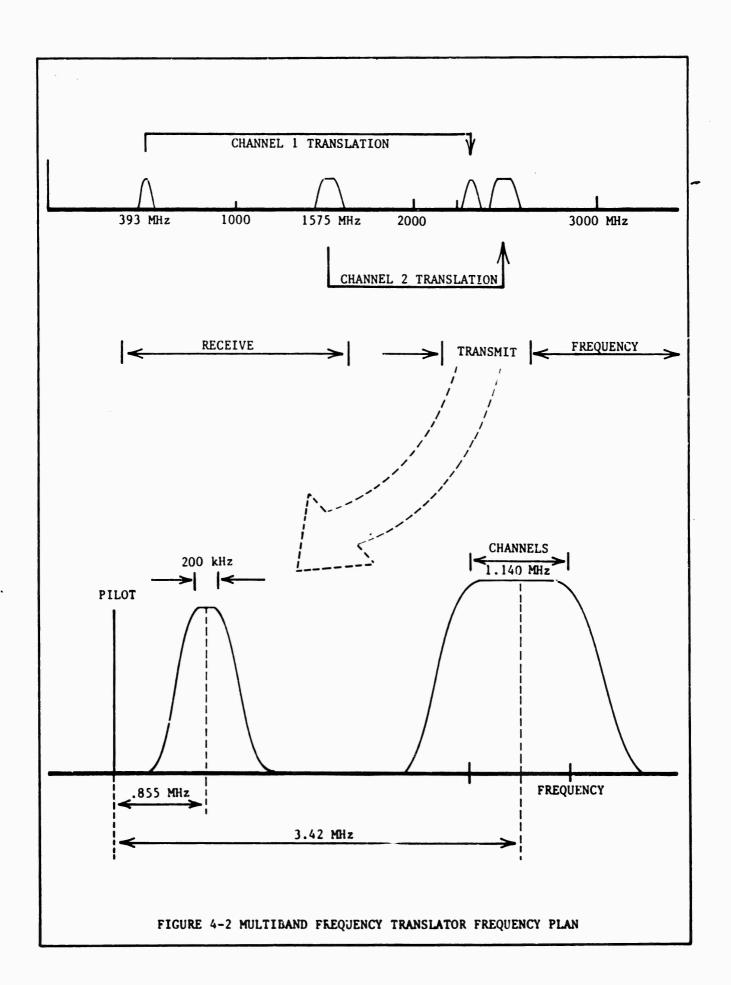
Additionally, the ground station transmits a low UHF signal to the aircraft which is also transponded back to the ground station at S-Band. This signal permits the recording of the doppler frequency shift. (Alternately, a PN sequence can be utilized on the turnaround channel to permit range and range rate determination).

The transponder, in addition to having a UHF transponded channel and the C/A transponded channels, has a beacon carrier. This beacon channel can be amplitude modulated with aircraft flight data.

The transponder described is being developed for missile tracking and should be well suited to this BSS application. Figure 4-2 shows the frequency translation of this Multiband Frequency Translator.







As an alternate to the UHT, a time-gated or CW signal can be used at L1. STI has recently completed a GPS study for this type of operation. The recommended codes have been less than -40 dB cross-correlation with respect to the GPS C/A codes.

## 4.2 System Characteristics

Figure 4-3 shows the information flow for this alternative. Satellite navigation data, aircraft telemetry (dynamics), and the ground originated navigation data provide the data base for assessing the aircraft's position. This data is totally independent of the aircraft's navigation system. The prime aircraft modification is to add an antenna/preamp on the aircraft frame for the reception of the NAVSTAR signals.

No X-set is required in the aircraft for the position determination; an X-set at the ground terminal serves this function. There is also the potential of deleting a time standard in the pod instrumentation, especially if ground ranging is utilized. A tabulation of Alternative C impact on the aircraft is given in Table 4-4.

This alternative also has potential advantage in that it is feasible to accomplish real time BSS processing at the ground station through the addition of a processor.

Because only the C/A Ll signal can be transponded by the aircraft, the ground terminal must use interpolation from its direct Ll/L2 signals to reserve the transponded signal's ionspheric propagation error. Because the spacecraft/ground geometry does not significantly change between the satellite to ground terminal and the satellite to aircraft, little error is expected in the interpolation. The nominal terrestrial range with a 5000 ft. aircraft altitude is approximately 80 nautical miles.

A ROM cost estimate has been made for this alternative C and this data is given in Table 4-5.

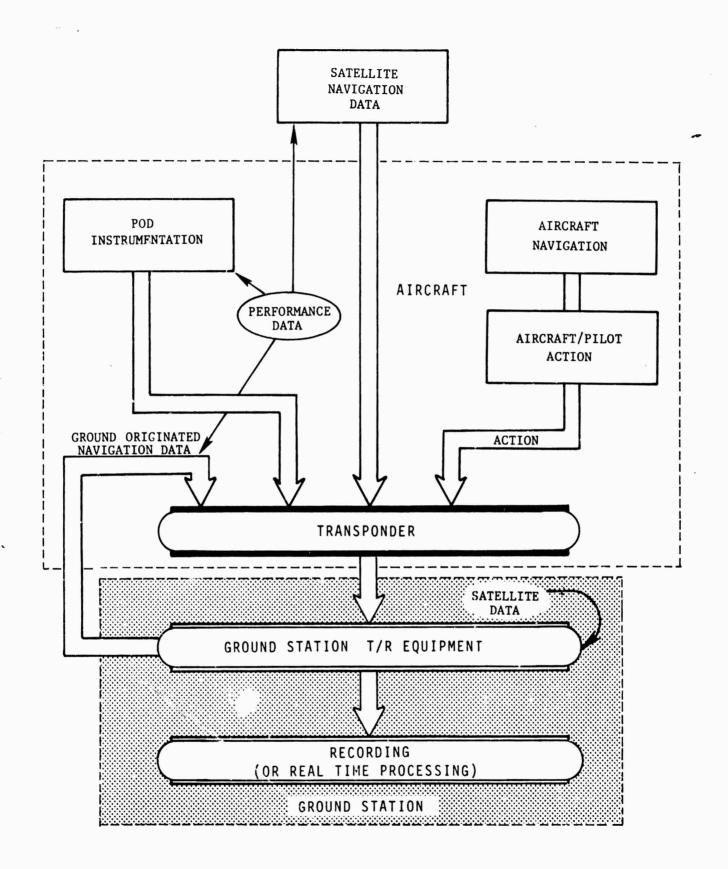


FIGURE 4-3 ALTERNATE C INFORMATION FLOW

TABLE 4-4
ALTERNATE C CHARACTERISTICS

			= 1	<del>*</del>	
WT	•	VOI	٠.	POWE	CR
15 1	bs	350	in <sup>3</sup>	1.5	watts
65 1	bs			150	watts
34 1	bs	1,496	in <sup>3</sup>	100	watts
2 1	bs	12	in <sup>3</sup>	1	watt
15 1	.bs	1,250	$in^3$	15	watts
15 1	.bs	350	$in^3$	2	watts
131 1	bs	5,864	in <sup>3</sup>	268	watts
35 1	.bs	2,000	$in^3$	200	watts
40 1	.bs			10	watts
206 1	bs	10,864	$in^3$	478	watts
30 1	.bs				
236 1	.bs				
250 1	.bs				
35 1	.bs				
521 1	.bs			478	watts
536 1	.bs			480	watts
	15 1  65 1  34 1  2 1  15 1  15 1  131 1  35 1  40 1  206 1  30 1  236 1  250 1  35 1  521 1	WT.  15 lbs  65 lbs 34 lbs 2 lbs 15 lbs 15 lbs 15 lbs 131 lbs 35 lbs 40 lbs 206 lbs 30 lbs 236 lbs 250 lbs 35 lbs 521 lbs	15 lbs 3,456 34 lbs 1,496 2 lbs 12 15 lbs 1,250 15 lbs 350 131 lbs 5,864 35 lbs 2,000 40 lbs 3,000 206 lbs 10,864 30 lbs 236 lbs 250 lbs 35 lbs 521 lbs	15 lbs 350 in <sup>3</sup> 65 lbs 3,456 in <sup>3</sup> 34 lbs 1,496 in <sup>3</sup> 2 lbs 12 in <sup>3</sup> 15 lbs 1,250 in <sup>3</sup> 15 lbs 350 in <sup>3</sup> 131 lbs 5,864 in <sup>3</sup> 35 lbs 2,000 in <sup>3</sup> 40 lbs 3,000 in <sup>3</sup> 206 lbs 10,864 in <sup>3</sup> 30 lbs  236 lbs 250 lbs 35 lbs 521 lbs	15 lbs 350 in <sup>3</sup> 1.5  65 lbs 3,456 in <sup>3</sup> 150 34 lbs 1,496 in <sup>3</sup> 100  2 lbs 12 in <sup>3</sup> 1  15 lbs 1,250 in <sup>3</sup> 2  131 lbs 5,864 in <sup>3</sup> 268  35 lbs 2,000 in <sup>3</sup> 200  40 lbs 3,000 in <sup>3</sup> 10  206 lbs 10,864 in <sup>3</sup> 478  30 lbs  236 lbs 250 lbs 35 lbs 478

TABLE 4-5

ALTERNATE C

ROM COST IMP. CT - VEHICLE

	NON-RECURRING	RECURRING
AIRCRAFT		
Ant/Install.	\$ 50,000	\$ 10,000
Preamp/Install.		15,000
Integ/Doc.	20,000	
Test	10,000	5,000
BSS POD		
Multiband Translator		35,000
IMU	10,000	25,000
Multiplexer/Modulator	40,000	20,000
OAT/SCA		10,000
Preamp (UHF)		5,000
ECU	50,000	20,000
PS System/Panel	25,000	20,000
POD Modif/Doc.	50,000	20,000
Integ/Install/Test	15,000	25,000
AGE	100,000	-
AUL		
TOTAL (VEHICLE)	\$370,000	\$210,000

TABLE 4-5 (Continued)
ALTERNATE C
ROM COST IMPACT-GROUND TERMINAL

GROUND TER	MINAL	NON-RECURRING	RECURRING
X-Set &	Antenna		\$150,000
X-Set			150,000
Transla	tor	\$ 25,000	10,000
Ranging	,	25,000	15,000
UHF Sou	ırce		10,000
MUX		40,000	15,000
IRIG TR	lG .		20,000
DTRS		10,000	25,000
Ant/Tra	icker	5,000	25,000
Shelter	Modif.	25,000	10,000
Integ/I	Install/Doc.	75,000	75,000
P.S. Sy		5,000	25,000
Test		20,000	25,000
		\$230,000	\$555,000
SYSTEM			
Test		40,000	25,000
TOTALS	(Vehicle)	370,000	210,000
	(G.T.)	230,000	555,000
	Test	40,000	25,000
		\$640,000	\$790,000

#### SECTION 5

#### 5.0 ALTERNATE COMPARISON & RECOMMENDATIONS

### 5.1 Comparison

A tabulation and comparison of key features of the three alternatives is given in Table 5-1. Alternate A appears to have the minimum impact on aircraft weight and power, can utilize a smaller pod, and is the least costly, however, it is also the least flexible in that it is only applicable to X-set equipped aircraft. It also provides the least independent data for scoring assessment.

Alternative B has the highest weight and power impact on the aircraft, requires a larger pod, and also appears to be the most costly. However, it is a flexible approach since it is applicable to any aircraft evaluation (not just those equipped with the GPS navigation system) and does not have a range limitation. For those applications where the prime mission navigation equipment is also in a pod, there could be a mounting conflict for the BSS pod.

Alternative C is also quite flexible in that it is applicable to any aircraft, it minimizes the equipment required in the instrumentation pod and can utilize a smaller pod. It further has the added potential of being able to accomplish <u>real time</u> bomb scoring through the addition of a processor at the ground terminal. The prime disadvantage of the system is that it is range restricted in that the aircraft and ground station must be in sight of each other. It furthermore requires a ground terminal, however, the ground terminal can easily be packaged to be air transportable.

An alternate A or B selection may also force a selection of A and B. Since alternate A is only applicable for X-set equipped aircraft, alternate B may then be required to score non - X-set equipped aircraft. Similarly, with an alternate B selection, if an aircraft is provided its navigation data from equipment mounted in a pod, then a second pod location is required for the BSS and may force the use of the smaller alternative A for this application where two large pods could not be accommodated by the aircraft.

Unlike alternatives A and B, alternative C requires only a small pod and is independent of the equipment on the aircraft. Additionally, the cost to implement an A and B pod, or two B pods is approximately the same in cost as implementing two C pods.

# 5.2 Recommendations

- 1. Because alternate C (transponded signals to a ground station):
  - a) requires one-third weight, power, and volume (compared to alternate B)
  - b) is less costly when more than one pod is implemented, (compared to alternate B)
  - c) has the potential for real time bomb scoring assessment, and
  - d) is applicable to any aircraft,

It is recommended that alternate C be implemented for the Bomb Scoring System.

2. Because alternate A is only applicable to X-set equipped aircraft, it is not recommended for implementation. This alternative could require that other alternatives also be implemented for the Non-X-Set equipped aircraft at a higher total system cost.

Ch	Characteristics	Alternate A (X-Set Equipped A/C)	Alternate B (X-Set in BSS Pod)	Alternate C (Transponded Signals to G.T.)
PHYSICAL	Aircraft weight power size	430 lbs. 485 watts small pod	1135 1bs. 1515 watts large pod (600 gal)	536 lbs. 480 watts small pod
	Capable of Real Time Assessment	ou	ou	yes(added processor required)
TANC	Adaptable to wide variety of aircraft	no (must have X-set)	yes (must have capa- bility of carrying pod)	yes
OPERATIO	Independent of Target Location	yes	yes	no (Aircraft must be in range of ground terminal: 80 nmi at 5000 ft. altitude)
	Independent Assessment	no (uses same navigation data as aircraft)	yes	yes
<b><i>PERFORMANCE</i></b>	Ability to Resolve Ionos- pheric Propagation Errors	excellent	<b>e</b> xcellent	<pre>good (requires inter- polation from ground terminal/ satellite geometry to aircraft/satellite geometry)</pre>
J	1 Pod	\$550 K	\$1,190 K	\$1,430 K
so	2 Pods	\$715 K	\$1,735 K	\$1,665 K
0	3 Pods	\$880 К	\$2,280 K	\$1,900 K

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19. KEY WORDS (Continue on reverse side if necessary and identify by block number) SAC GPS transponder Bomb Scoring Systems Aircraft instrumentation			
GPS Range Instrumentation			
ABSTRACT (Continue on reverse side if necessary and identify by block number) This volume summarizes the work performed for the Bomb Scoring System using GPS Phase I.	Air Force addressing a GPS/SAC		
This report describes the evaluation and comparison (BSS) techniques which use the GPS satellites to a ment. The objective of each system is to provide	ssist in the accuracy assess-		

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Alternate A considers the use of on-board GPS and other aircraft instrumentation to derive the evaluation. Since it uses on-board equipment, alternate A has the least impact on the aircraft's performance. It is, of course, limited in its application to GPS-equipped aircraft.

Alternate B considers the use of totally redundant equipment, carried in a separate BSS pod to derive the independent assessment, and is similar in nature to the GPSTP.

Alternate C considers the use of transponded data to a ground station in order to minimize the aircraft-carried equipment, therefore minimizing the impact to the aircraft's performance.